

Calculation of marginal size:

$$\begin{aligned} \sigma_{\text{design}} &= \frac{\sigma_y}{1.5} && \text{for ductile material} \\ &&& \text{(under bending or tension)} \\ \text{or } \sigma_{\text{design}} &= \frac{\sigma_u}{3} && \text{for brittle material} \\ &&& \text{(under bending or tension)} \end{aligned}$$

$$\begin{aligned} P_{\text{design}} &= \text{Design Load.} \\ &= \text{Load} \times \text{relevant load factor} \end{aligned}$$

The calculated size is considered the min. size that can be used.

Allowance should be made for :

- Undercuts
- Change in surface quality
- provisions for mounting other components

Then : For static loading :

$$\text{Working stress} = \frac{\text{Actual Load (working Load)}}{\text{Adopted size cross section property}} \\ \text{(and considering stress concentration factor if any)}$$

$$\text{Working safety factor} = \frac{\text{Relevant Char. stress}}{\text{Working stress.}}$$

Load Factor

Loading condition	Load factor
- Manual operation	1.5
- Electric motor as a prime mover	
• Direct on line connection	2
• Star/Delta (Y/Δ) connection	$\sqrt{3}$
• Soft starter (Cent. Coupling, clutch, hyd. Coupling)	1.5
- Pressure Cyl. and pipes	
• unfired	1.5
• fired	2
- Testing of cranes and hoists:	
• Static test (limit deflection $\leq \frac{1}{300}$ span)	1.4
• Dynamic test	1.25
- Static load	1.0

Selected Material :

Brittle

Ductile

- * Characteristics considered for design according to type of load:

— Static σ_{ut} (bending stress) σ_y or $\sigma_{0.2\%}$
 τ_y

— Dynamic

- Completely reversed σ_{en}

- General:

Pulsating } σ_{ut}
Alternating } σ_{en}
($\tau \approx 0.6\sigma$) σ_{yt}
 σ_{end}

- * Margin of safety :

2.5 → 3

1.3 → 1.5

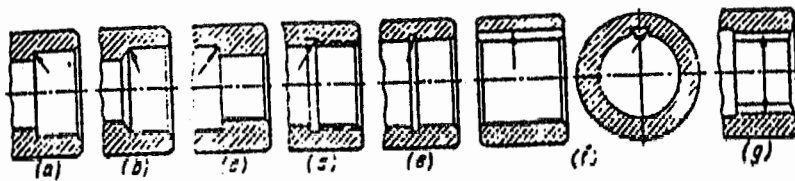
- * Stress concentration under static load:

- for material structure 1.25 → 1.5

- for geometry

Tables

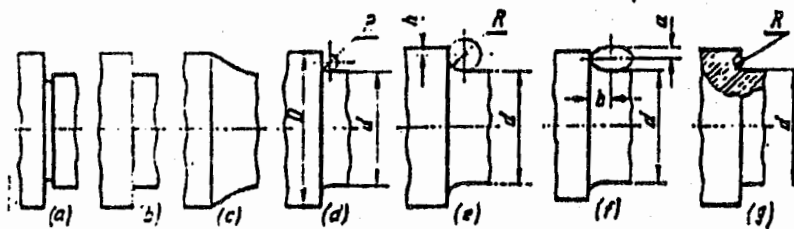
1.0



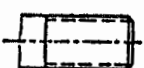
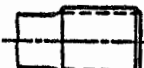
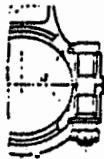

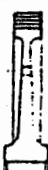
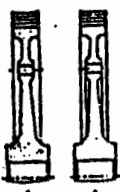
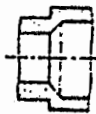
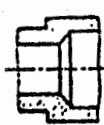


Stress concentrators in hollow shafts (indicated by arrows)

Stress Concentrators

Sketch	Concentrators	Sketch	Concentrators	Sketch	Concentrators
	Shallow drilled holes		Annular recesses		Key-ways
			Grooves		
			Sharp-angled stops		Splines
	Holes		Undercuts		Tooth spaces
	Threaded holes		Flats		End face slots
			Threads		
					Welds
					Marks

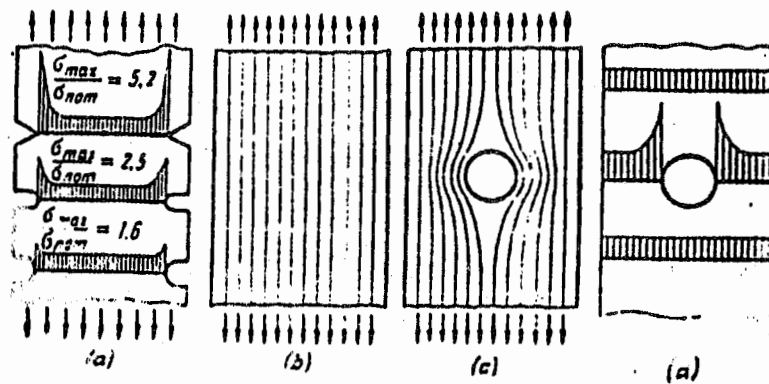


Decreasing stress concentrations in the entry angles of stepped shafts

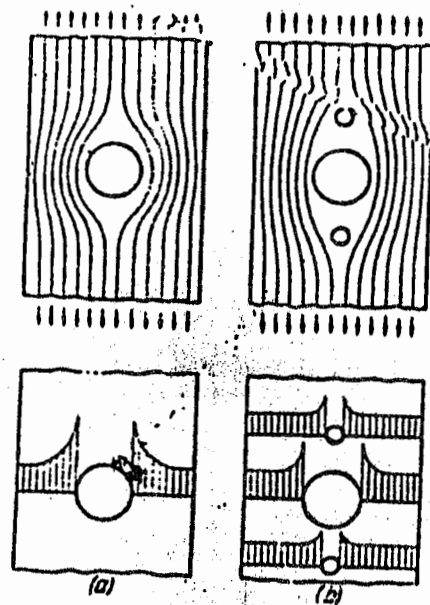
Original design	Improvement	Essence of improvement
<p>Screwed rod</p> 		Screwed portion enlarged
<p>Control big end</p>  <p>At positions <i>a</i> the part is weakened by bolt head and nut recesses</p>		Sectional areas of weakened portions enlarged
<p>Turbine rotor</p>  <p>Rotor disk weakened by relieving holes</p>		<p>1. Holes strengthened with bosses</p> <p>2. Holes positioned in a strengthening ring</p>
<p>Hollow shaft</p> 		Internal stress concentrator moved
<p>Two concentrators combine (external and internal entering angles)</p> 		Internal angles given smooth streamlined forms

Design Considerations

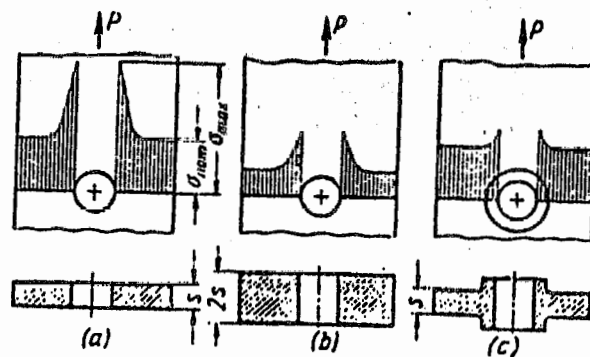
1. Stress Concentration Considerations:



Force flow in a part undergoing tension



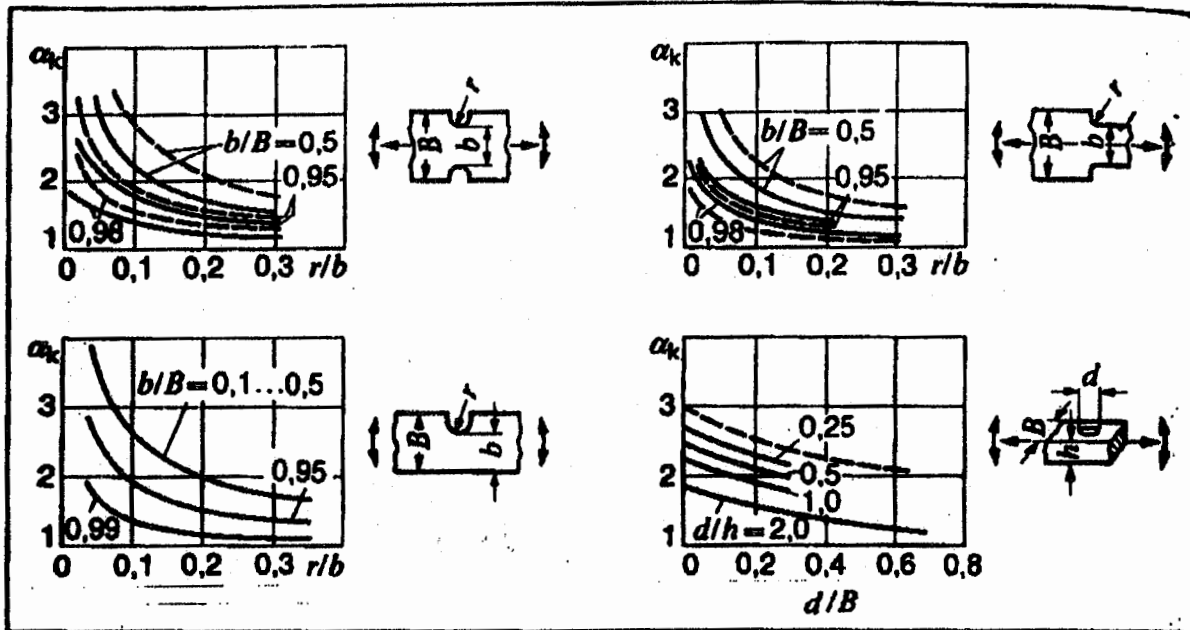
Force flow in parts
(a) with a stress concentrator (fillet); (b) with stress decelerations



Decreasing the maximum stress by lowering the nominal stress

Stress concentration factor α_k for various notch configurations

Stress Concentration Factors for Flat Bars



Stress Concentration Factors for Rods

